

# Study on Thermomechanical Treatment, Mechanical Properties and Fatigue of Nitinol Superelastic Thin Sheet

*Matthias Mertmann, Wolfgang Oswald*

*Memry GmbH, Weil am Rhein, Germany*

*Rainer Steegmüller, Andreas Schüssler*

*Admedes Schuessler GmbH, Pforzheim, Germany*

## Agenda:

- Introduction
- Experimental
- Mechanical Data & Fatigue
- Conclusions

# Introduction

- Nitinol in thin sheet form is gaining relevance in the market place:
  - Mass products successful such as Abbott StarClose™ and 3M SmartClip
  - More design variants for engineers
  - Possibility for OEMs to differentiate
  - New/different manufacturing processes, e.g. photochemical etching, stamping, deep drawing

# Introduction

- Nitinol sheet consumption is growing:
  - We expect today about 7`500 lbs worldwide
  - Still small if compared to Nitinol tube (ca. 100`000 lbs)
  - Number of vendors increases → competition + price pressure increase:
    - Nitinol tubing: ca. 12 manufacturers worldwide
    - Nitinol thin sheet: ca. 4 manufacturers worldwide

# Introduction

## Purpose of this Paper:

- Paper investigates the effect of thermomechanical treatments on the properties (mechanical, thermal, fatigue) of Nitinol thin sheet.
- Special emphasis is put on the effect of sheet anisotropy on mechanical properties

Sample manufacturing carried out at Memry GmbH/D

Tensile testing, DSC & Fatigue testing carried out at Admedes GmbH

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# Experimental

## Preparation of Sample Matrix:

- 3 different CW
- 5 different annealing temperatures
- 3 different annealing durations
- Sample orientation in  $0^\circ$  (RD),  $90^\circ$  (TD) and  $45^\circ$  to rolling direction
- Final sheet thickness constant (0.3 mm)

# Experimental

## Sample Matrix:

Parameter	Value
Cold Work	25% - 30% - 35%
Heat treatment temperature	480°C - 495°C - 510°C - 525°C - 540°C
Heat treatment duration	3 min. - 3 + 8* min. - 3 + 28* min.
Sample orientation	RD - TD - 45°

\*: time in air convection furnace after flat annealing

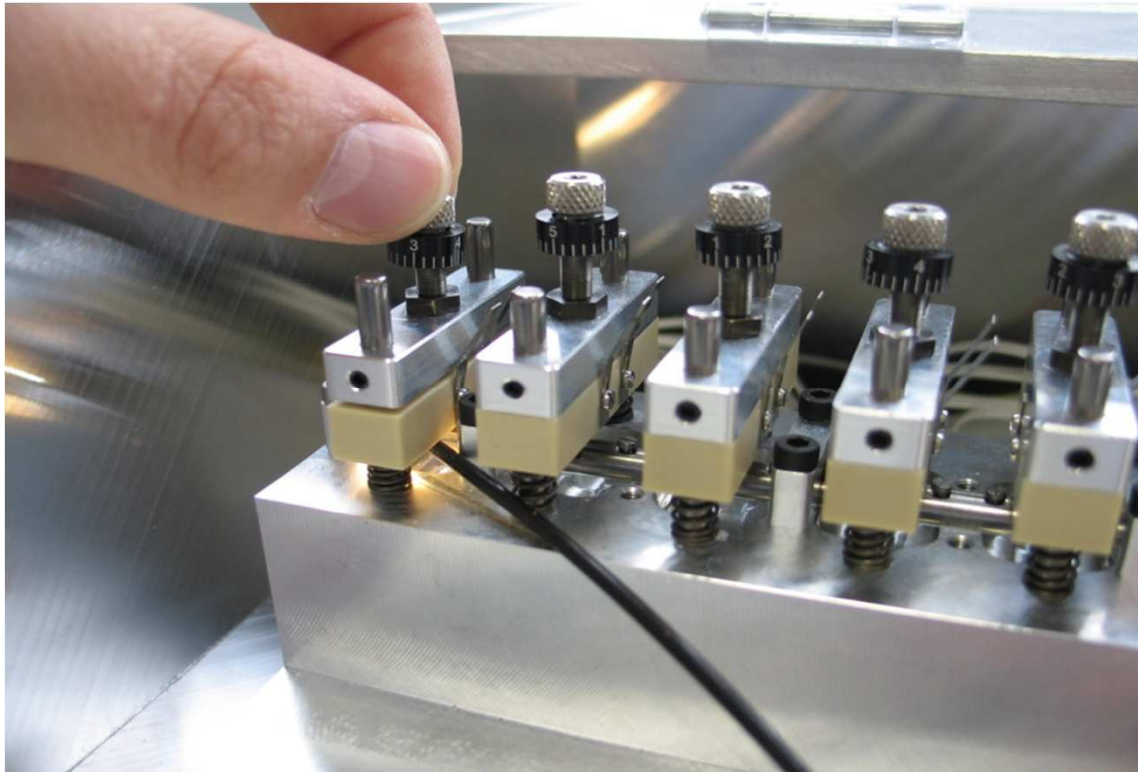
# Experimental

## Test Matrix:

- Tensile testing ( $T = 37^{\circ}\text{C}$ ) → ASTM F2516
- DSC testing → ASTM F2004
- Bend-and-Free recovery testing → ASTM F2082 (BFR)
- Fatigue testing ( $T = 37^{\circ}\text{C}$ )

# Experimental

## Fatigue Tester:



Admedes Fatigue Tester:

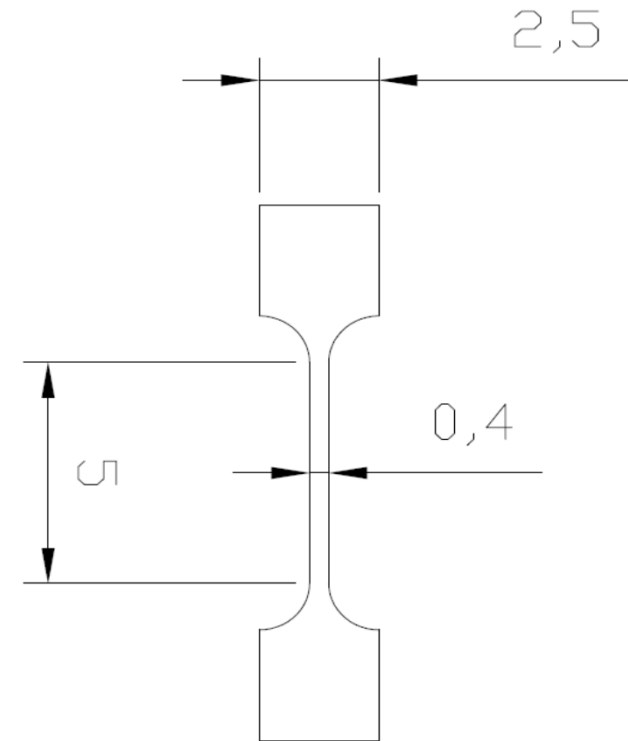
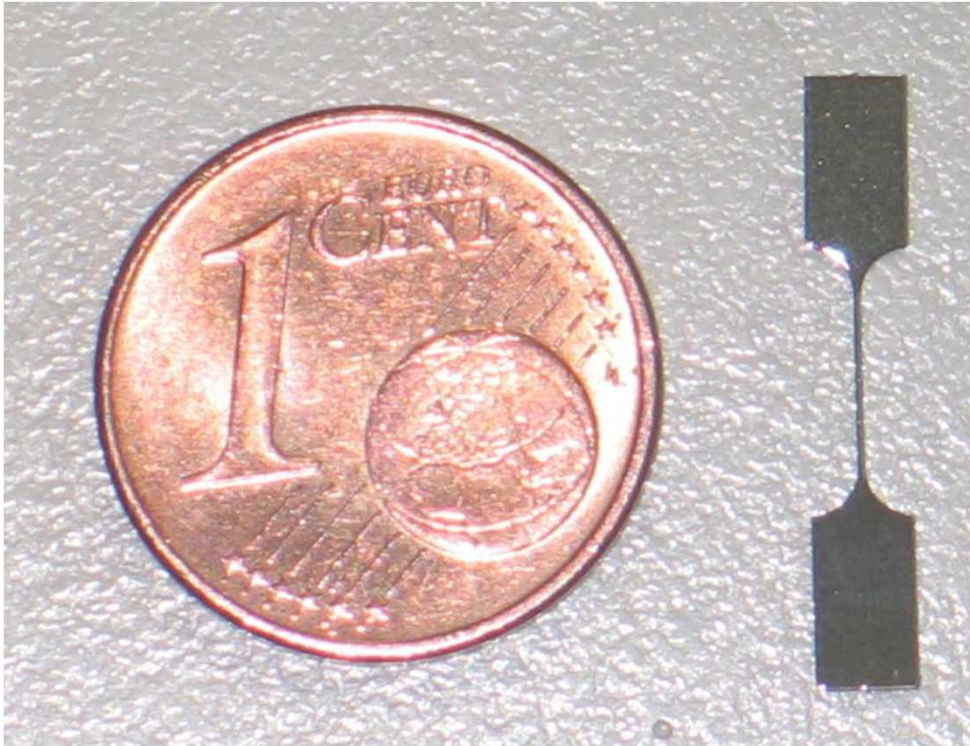
- 3-point bending mode
- Air convection
- High frequency (60 Hz)
- 10 identical samples
- Test stop when fracture occurs

# Experimental

## Sample preparation:

- Laser cutting of  $\mu$ -Dogbones
- Deburring
- EP surface finish

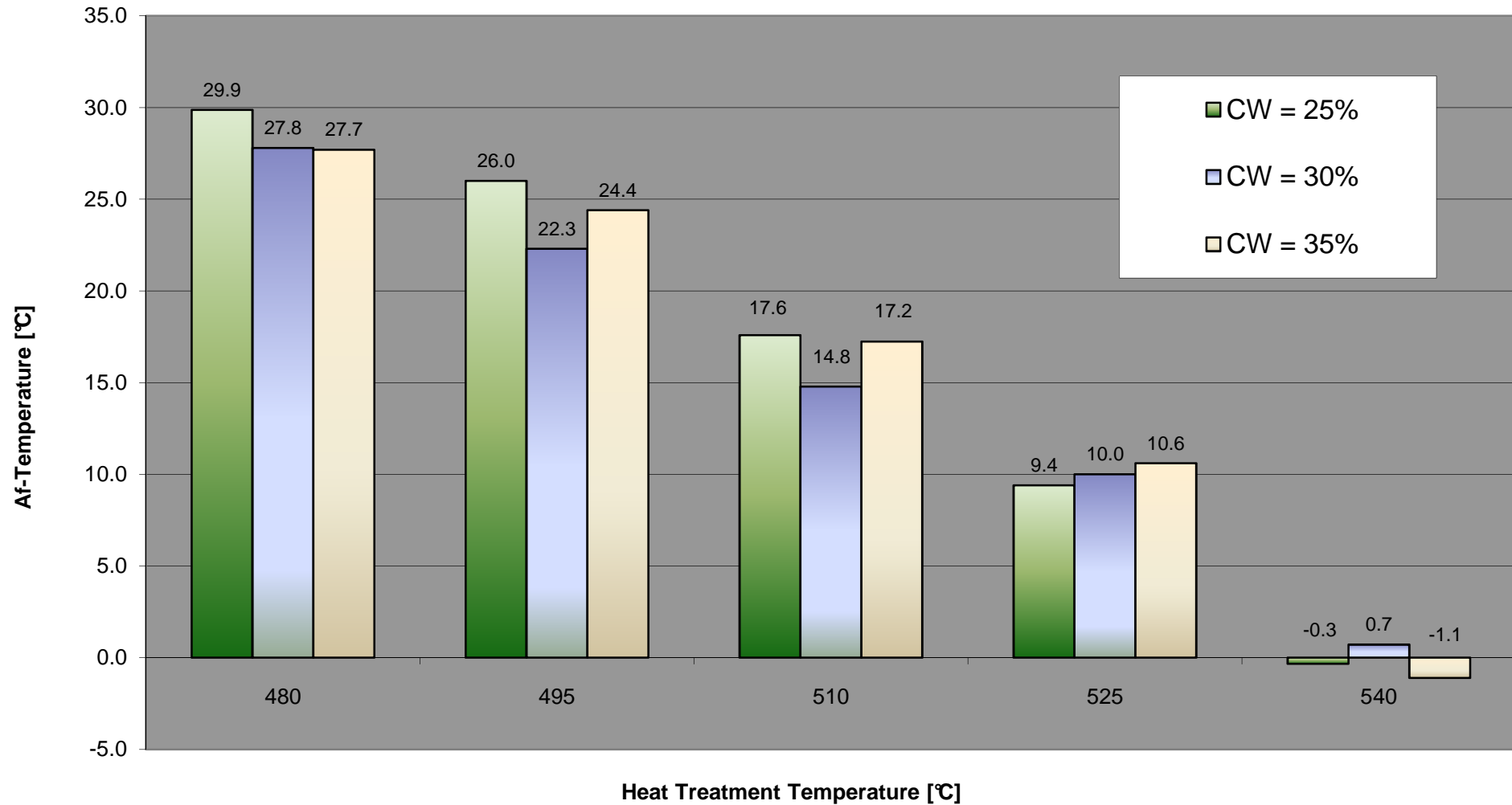
# Experimental



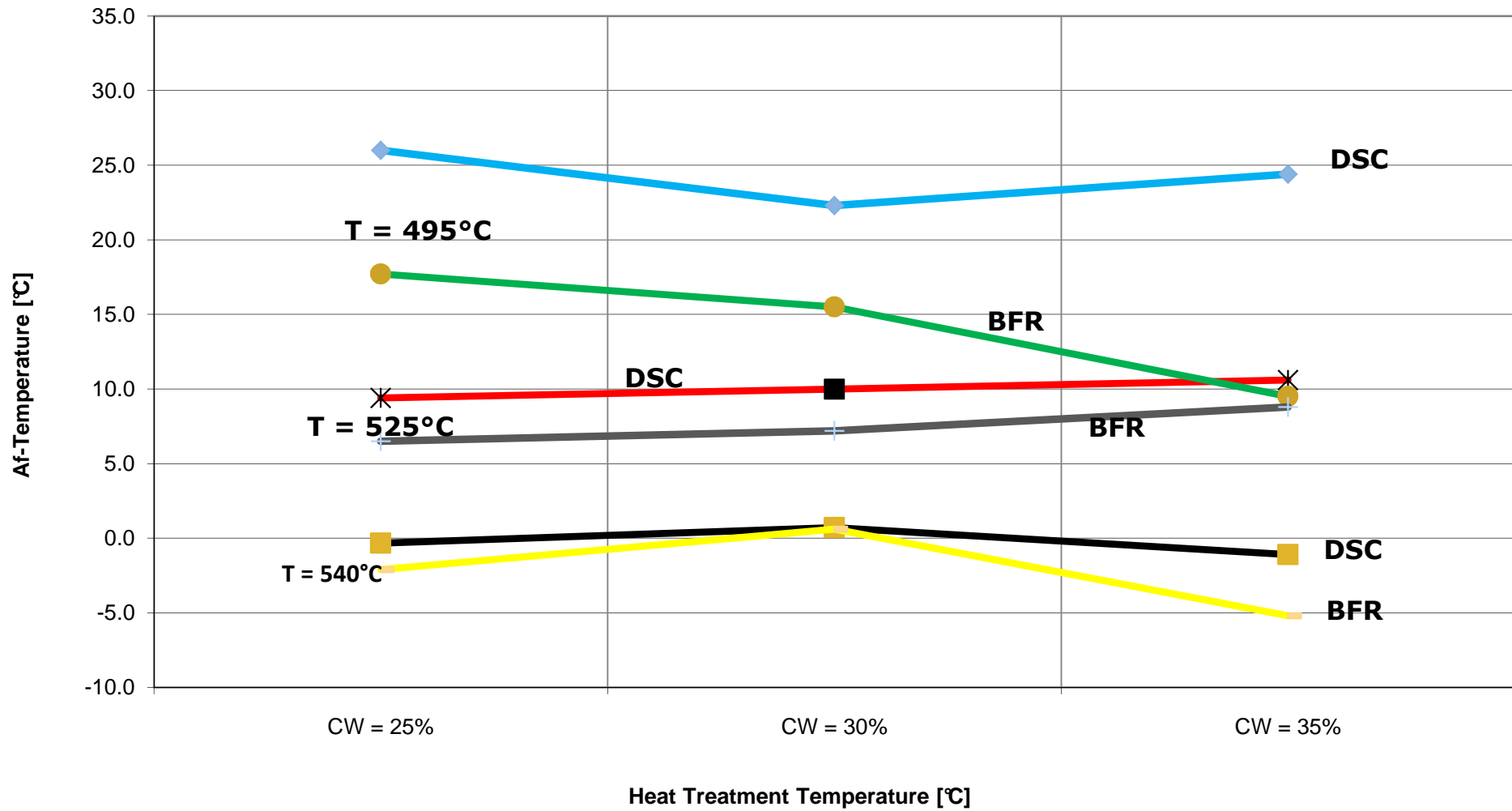
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# Results: DSC & BFR



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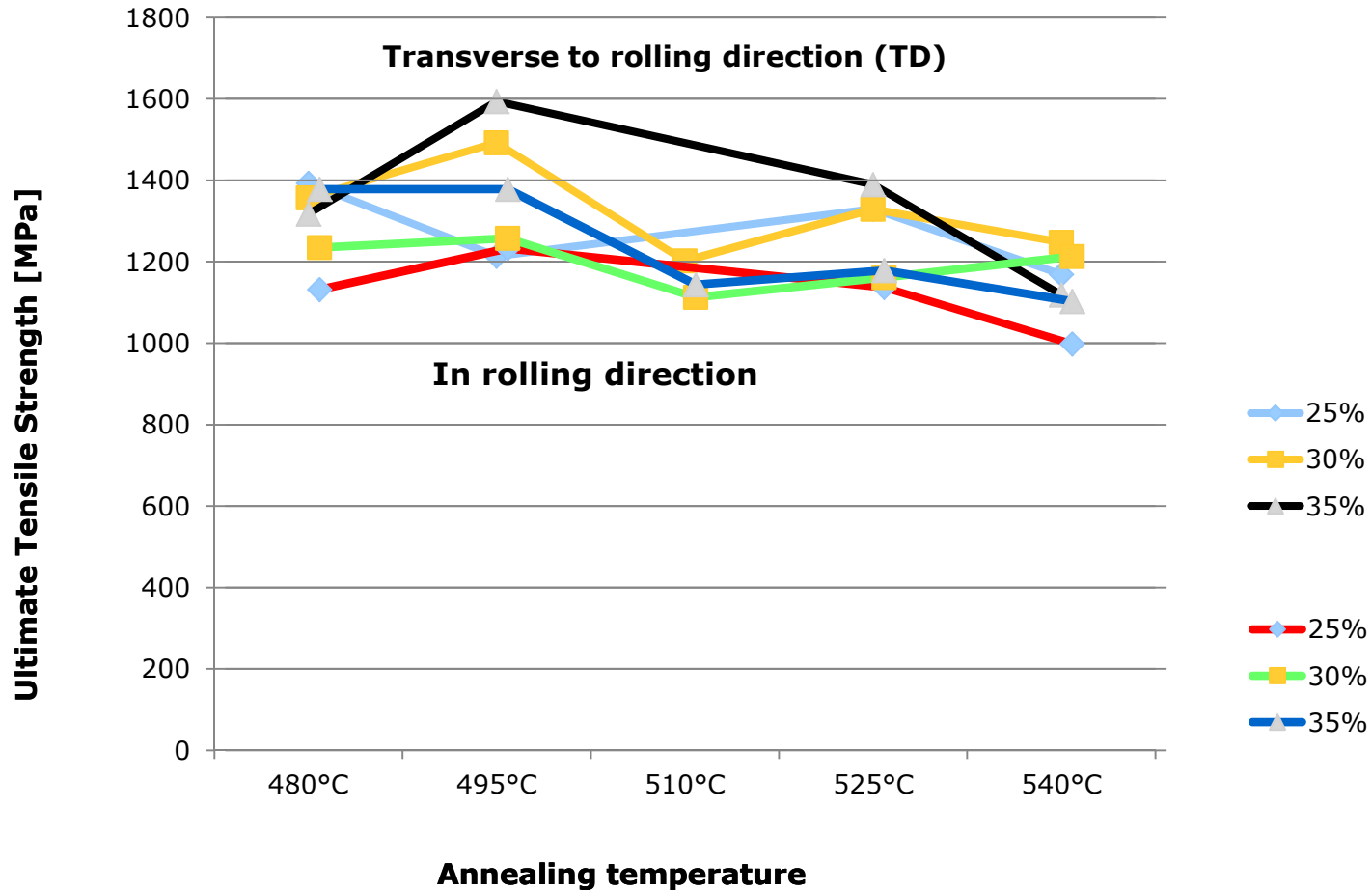


# Results: DSC & BFR

## Key Findings:

- DSC results were in line with data collected from wire with similar test parameters
- Differences between the investigated CW-% were minor/insignificant
- Correlation between DSC and BFR acceptable only for higher annealing temperatures

# Results: Tensile Tests



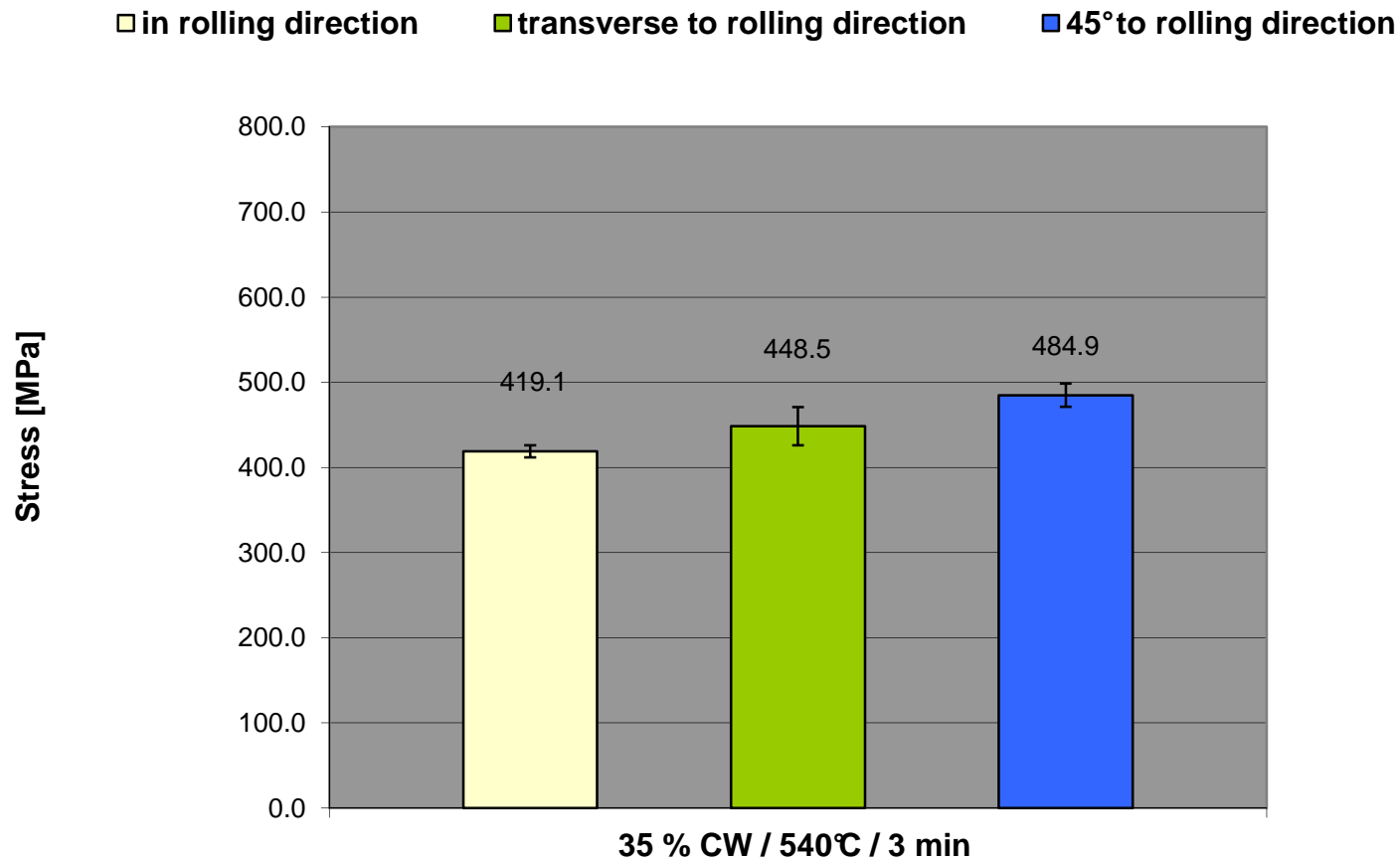
# Results: Tensile Tests

## Key Findings:

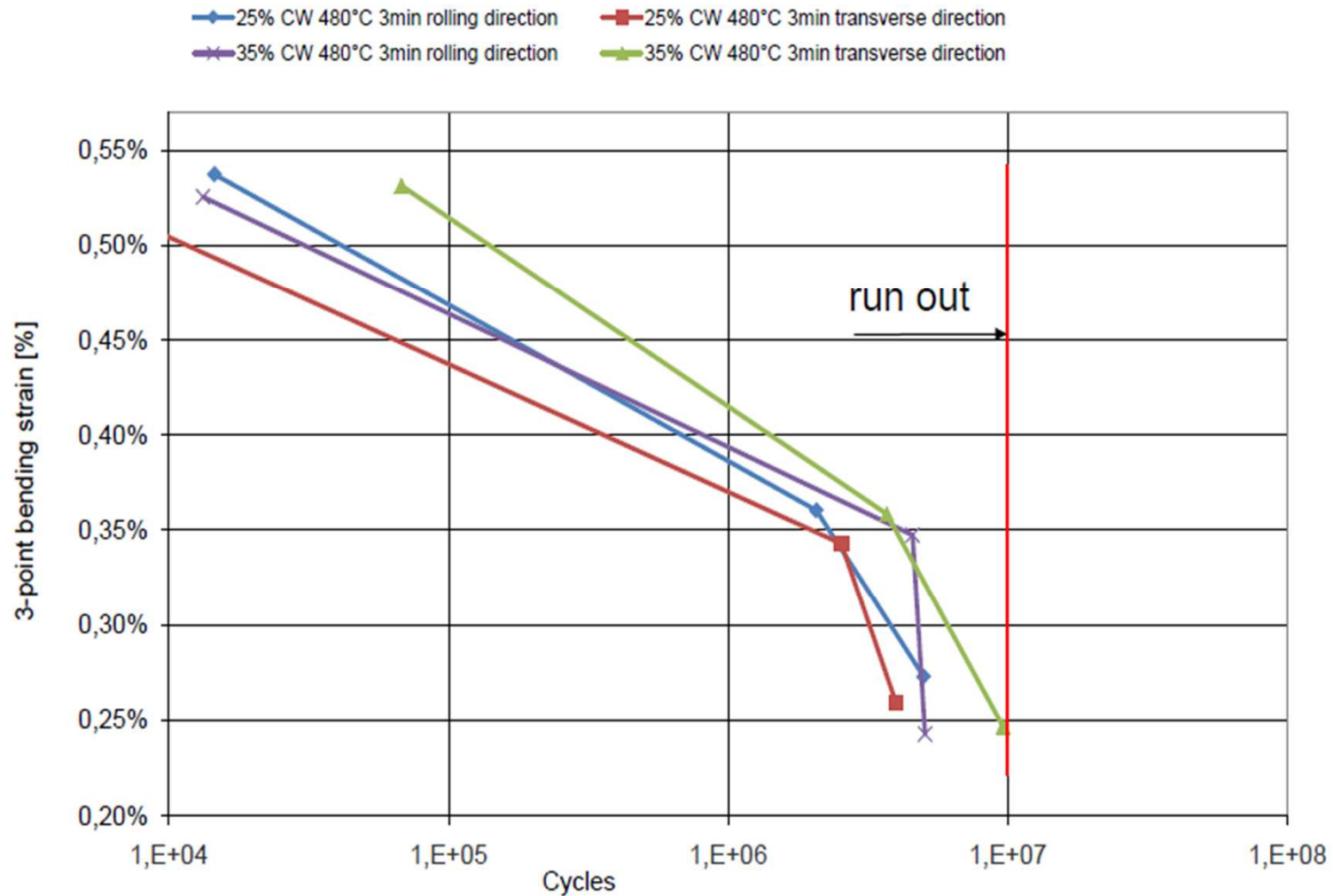
- UTS values tend to be higher for TD as compared to RD → smaller grain size
- Plateau stresses tend to be higher in TD. Most likely: energy level to activate martensite variants is different in different crystallographic orientations
- 45° orientation shows highest plateau stresses!

# Results: Tensile Tests

## Upper Plateau Stress vs. Sample Orientation



# Results: Fatigue Tests



# Results: Fatigue Tests

## Key Findings:

- 3-point bending fatigue tests did generate only few run-outs
- No clear difference between TD and RD!
- High test frequency eventually affected the test results

# Conclusions

## Key Takeaways:

- Results on Nitinol thin sheet are similar to wire/tube
- UTS in TD higher than in RD
- Plateau in 45°C higher than RD/TD
- DSC does not show big effect of CW on Af

# Acknowledgement

Special thanks to Admedes staff:

- Dr. Rainer Steegmüller
- Michael Quellmalz
- Wolf-Dieter Stephan

for performing most of the testing and discussions